



SPAD Image Sensors for Quantum and Classical Imaging

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ABSTRACT

Single-photon avalanche diodes (SPADs) have been demonstrated on a variety of CMOS technologies since the early 2000s. While initially inferior to their counterparts implemented dedicated technologies, modern CMOS SPADs have recently matched them in sensitivity, noise, and timing jitter. Indeed, high time resolution, enabled by low jitter, has helped demonstrate the most impressive developments in fields of imaging and detection, including fluorescence lifetime imaging microscopy (FLIM), Förster resonance energy transfer (FRET), fluorescence correlation spectroscopy (FCS), time-of-flight positron emission tomography (TOF-PET), and light detection and ranging (LiDAR), just to name a few. The SPAD's power of detecting single photons in pixels that can be replicated in great numbers, typically in the millions, is currently having a major impact in computational imaging and quantum imaging. These two emerging disciplines stand to take advantage of larger and larger SPAD image sensors with increasingly low jitter and noise, and high sensitivity. Finally, due to the computational power required at pixel level, power consumption must be reduced; we thus advocate the use of in situ computational engines, which, thanks of CMOS' economy of scale and 3D-stacking, enable vast computation density. Some examples of this trend are given, along with a general perspective on SPAD image sensors.

1.0 INTRODUCTION

A single-photon avalanche diode (SPAD) is a reverse-biased photodiode operating above breakdown voltage, a regime generally referred to as Geiger mode of operation [1]. Thus, SPADs are often called Geiger-mode avalanche photodiodes (GM-APDs). Due the high electric fields in play, designed to achieve impact ionization, a conventional planar photodiode needs to be modified, so as to prevent premature edge breakdown.



Figure 198-1: Generic SPAD cross-section and operation.

The figure above shows the typical cross-section of a SPAD and the biasing regime to achieve Geiger mode of operation, thereby enabling virtually infinite optical gain and thus single-photon detectability. The figure also shows important parameters, such as the breakdown voltage (V_B) and excess bias voltage (V_E), i.e. the voltage in excess of the breakdown used for biasing the SPAD. To avoid the destruction of SPADs, it is necessary to quench the avalanche as quickly as possible and to recharge the device to its original idle voltage. The figure below describes a possible scheme, known as passive quenching, that can be used for this



purpose. Other schemes, involving active quenching and/or recharge, are also known in the literature. It is important to note that fast quenching can have positive implications in the reduction of afterpulsing and timing jitter, but also in long-term reliability of SPADs. Fast recharge mostly reduces dead time, which in turn increases the maximum photon flux one can detect; it can also be used to control afterpulsing probability [2-4].



Figure 198-2: SPAD passive quenching and conversion to a digital signal.

A CMOS SPAD can achieve today sub-10ps timing resolution, measured as single-photon time resolution (SPTR) [5,46,47], while recently SPADs have reported sensitivity, measured as photon detection probability (PDP), as high as 90% [42]. Photon detection efficiency (PDE) is often reported and it is defined as PDP×FF, where FF denotes the fill factor, i.e. the ratio between active area and total area of the pixel. Another important performance measure for SPADs is dark count rate (DCR), which relates to counts measured in the SPAD in the dark on average [6-8]. With the introduction of CMOS SPADs in 2003 [9], new scalable devices have appeared, with the possibility of integrating thousands or millions on the same chip [10-14]. New performance measures have thus emerged, which relate to large arrays, such as crosstalk both of optical and electrical nature, and the uniformity of performance measures, such as dead time, PDP/PDE, DCR, and SPTR. Uniformity is usually defined in %-variation over the area of the chip, and it is usually a function of technology, temperature, and excess bias voltage.

To achieve large-format SPAD image sensors, it was necessary to scale SPADs down to smaller dimensions, so as to achieve small pitch pixels. This required the development of SPADs in deep-submicron CMOS technologies. Over the years, 180-nm, 160-nm, 150-nm, 130-nm, 110-nm, 65-nm, 55-nm, and 40-nm SPADs were thus created [15-25], whereas SOI SPADs [20], p-i-n SPADs [21], and subsequently backside-illuminated (BSI) SPADs were developed to enable 3D-stacking, which was introduced in 2015 [26]. With 3D-stacking it was now possible to implement complex functionality back-to-back with the SPADs. Moreover, SPAD optimization could now be decoupled from logic and mixed-signal design miniaturization, thus enabling further improvement of density. As a result, a flurry of applications of SPADs appeared in the biomedical [27,28] field, in LiDAR [29], and many other applications requiring time-resolved imaging, including a new emerging field of research: quantum imaging [30].

Thanks to all these advances, in the mid-2010s, researchers began increasing pixel counts [31] to achieve the megapixel milestone in 2020 [32]. 3D-stacking and BSI SPADs advanced as well, with the creation of architectures that could enable higher excess bias and thus higher PDE and better SPTR [33]. Moreover, research on high-dynamic range imaging could yield a better understanding of SPAD operation, especially at low and high illumination regimes [34,35]. New materials are available today for the extension of SPAD PDE, especially in the near infrared spectrum [36], along with more advanced models thanks to a deep understanding of the physics of avalanching [37-41] as well as alternative methods to detect single photons [40]. Even traditional CMOS SPADs have continued to advance and have now become commonplace in consumer electronics [43-47]. The table below summarizes recent achievements in CMOS SPADs in terms of the performance measures described above.





Comparative Table									
	Technology	Diameter	V_{EX}/V_{BD}	Peak PDP	PDP (%)	DCR/unit area	AP (%)	Jitter (ps)	FoM _T [44]
	(nm)	μm	(V)	(%) $@\lambda$ (nm)	@850 nm	$(cps/\mu m^2)$			
Ghioni [7]	Custom Thin	50-200	5-10/30-35	52-68 @550	12-15	$0.4 - 1.6^{a}$	2^{b}	35 ^c	1.88E+11
Gulinatti [8]	Custom RE	50	20/45-55	58 @650	28	0.3^{d}	N/A	93 ^c	N/A
Villa [16]	350	10-500	2-6/25	37-53 @450	2-4.5	0.05^{a}	1^e	90^{f}	6.52E+11
Leitner [17]	180	10	1-3.3/21	35-47 @450	N/A^g	0.3-1.8 ^a	N/A	N/A	N/A
Veerappan [18]	180	12	2-10/23.5	24-48 @480	3-8	$0.16-176^{a}$	$0.03-0.3^{h}$	$112-88^{i}$	1.37E+9
Veerappan [19]	180	12	1-4/14	23-47 @480	4-7	$0.28-16^{d}$	0.2^{j}	$161 - 141^{i}$	2.78E+9
Veerappan [21]	180	12	1-12/25	18-47 @520	2-8	$0.2-6^{d}$	7.2^{k}	139-101 ⁱ	5.88E+9
Xu [22]	150	10	2-5/19	24-32 @450	2-3.5	0.1-1	$1 - 13^{l}$	42^{m}	1.33E+11
Lee [20]	140(SOI)	12	0.5-3/11	12-25 @500	2.5-7	0.9-260	1.7^{n}	65°	1.17E+9
Richardson [13]	130	8	0.6-1.4/14	18-28 @500	3-5	$0.24-0.6^{a}$	0.02^{p}	200^{q}	9.04E+9
Richardson [12]	130	8	0.2-1.2/12-18	18-33 @450	2-5	0.4-0.8	0.02^{r}	237-184 ^s	4.01E+10
Niclass [10]	130	10	1-3.5/10	31-41 @450	3	$120-1300^{d}$	N/A	144^{i}	N/A
Niclass [43]	180	25	5/20.5	$64.8 \ @610^{ii}$	24	0.6	0.49^{dd}	190	1.83E+11
Gersbach [11]	130	4.3	1-2/9	18-30 @480	3.5-5	1.5-11.5	<1 ^t	125^{i}	3.89E+9
Charbon [15]	65	8	0.05-0.4/9	2-5.5 @420	0.2-0.4	340-15.6k ^a	$<1^{u}$	235^{i}	3.71E+5
Sanzaro(A) [24]	160(BCD)	10-80	3-9/36	31-58 @450	2.5-6.5	$0.12 - 0.2^{v}$	$0.43 - 1.59^w$	39-28 ^c	9.12E+11
Sanzaro(B) [24]	160(BCD)	10-80	3-9/25	2-47 @450	2.5-6.5	$0.1 - 0.18^{v}$	$0.02 - 0.14^w$	36-28 ^c	7.9E+11
Sanzaro(C) [24]	160(BCD)	10-80	3-9/26	55-71 @490	6-9	$0.13 - 0.19^{v}$	$0.41 - 1.26^{w}$	41-28 ^c	1.15E+12
Pellegrini [25]	40	18.36	1/15.5	45 @460+	5	N/A^{\dagger}	0.1	170^{*}	N/A
Nolet [5]	65	20	1.75/9.9	8 @470	N/A	2.8k	<10	7.8 [#]	N/A
Webster [14]	90	6.4	14.9/2.4	44 @700	22	8.1k	0.375	84	N/A
This Work	180	25-100	1-11/22	$25-55@480^2$	3-8.4 ^x	0.06-0.23 ^y	\sim 0.12-3 z	12.1^{1}	2.78E+13

Table 198-1. Summary of SPAD performance [46].

^a At 20°C.^b 200 μ m-diameter, at 25°C, 80 ns dead time, V_{EX}=5V.°820 nm wavelength.^d At 25°C.^{dd} 24 ns dead time.^e 30 μ m-diameter, at 25°C, 40 ns dead time, V_{EX}=5 V, integrated AQC. ^f A time resolution of 28-37 ps FWHM and a diffusion tail of 160-340 ps were demonstrated in Ref. [45] using the substrate bias as a trade-off parameter between jitter and diffusion tail.^g PDE=10-13% at 800 nm.^h 300 ns dead time, V_{EX}=2-10 V.ⁱ 637 nm wavelength.ⁱⁱ Substrate not isolated SPAD. ^j 300 ns dead time, V_{EX}=2V.^q 815 nm wavelength.^r 50 ns dead time, V_{EX}=1.5-5 V.^m 831 nm wavelength.^h 200 ns dead time, V_{EX}=2V.^q 405 nm wavelength.ⁱⁱ 100 ns dead time.ⁱⁱ 410 ns dead time.ⁱⁱ 4130 ns dead time.ⁱⁱ 4130 ns dead time.ⁱⁱⁱ 4130 ns dead time.ⁱⁱⁱ 4130 ns dead time.ⁱⁱⁱ 4130 ns dead time.ⁱⁱⁱ 414 ns and 6 V excess bias.ⁱⁱ For a dead time of 3 ns on the 25 μ m-diameter at 20°C with an excess bias.ⁱⁱⁱ 1 V excess bias.ⁱⁱⁱ 410 nm laser.ⁱⁱⁱ 420 nm laser.ⁱⁱⁱ 420 nm laser.ⁱⁱⁱⁱ 420 ns deavet in the superature at 20°C with an excess bias of 6V.² value taken at 1 V and 6 V excess bias.ⁱⁱⁱ 410 nm laser.ⁱⁱⁱⁱⁱⁱ 410 ns deavet at 1 V and 6 V excess bias.ⁱⁱⁱ 410 nm laser.ⁱⁱⁱⁱⁱ 425 mm diameter at 20°C with an excess bias of 6V.² value taken at 1 V and 6 V excess bias.ⁱⁱⁱⁱⁱⁱⁱ

Recently, a number of SPAD imagers has also been used in quantum distillation [48], quantum LiDAR [49,50], and quantum plenoptic cameras [51], where pairs of entangled photons generated through spontaneous parametric downconversion (SPDC) are employed extract appropriate information from scenes suffering from extensive background illumination and challenging interpretation [52]. The figure below shows a micrograph of the first megapixel SPAD image sensor, MegaX [32].



Figure 198-3. The MegaX chip.

This sensor was employed in several classical applications, like the light-in-flight experiments, LiDAR imaging, and widefield FLIM, and quantum imaging applications, like quantum distillation and quantum LiDAR. Quantum imaging, though, requires not only single-photon detection, but also dedicated architectures enabling to use photogenerated pulses *in situ* or at least not to degrade the timing resolution of the detection. The principles and architectures recently emerged to implement quantum and classical imaging using SPAD sensors and the challenges of such implementations at system level focus on the promise of better resolution, PDE, DCR, and especially pixel count [52,53,54]. In addition, with the introduction of larger formats in SPAD imagers, several applications introduced earlier in the literature have been improved. This is so especially in the presence of massive radiation and background illumination. Examples are non-



line-of-sight imaging [54,55,56] and diffuse imaging [57,58]. At the same time, new imaging modalities, such as quanta burst photography (QBP) [59], quantum state tomography, and quantum holography are emerging. Researchers involved in these activities request multi-megapixel SPAD cameras, along with RGB and non-Bayer color filters for low-light illumination applications, as well as multi-spectral and hyper-spectral filter patterns. Similarly, reconfigurable SPAD sensors are sought to achieve solutions capable of adapting to various conditions of illumination and dynamic of the scene. One such example has recently been proposed in [60].

In conclusion, the field of single-photon imaging has found its application in a wide variety of imaging modalities, which require an increasingly rich set of specifications. Emerging computational imaging and quantum imaging are increasingly demanding larger formats and more computation *in situ*. This trend is opening the use of natively digital photodetectors, such as SPADs, to localized processing and artificial intelligence, which is currently under development and will be facilitated by the economy of scale of CMOS applied to SPADs, enabling lower power, higher functionality, and scalable designs. This is a clear trend for the future.

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